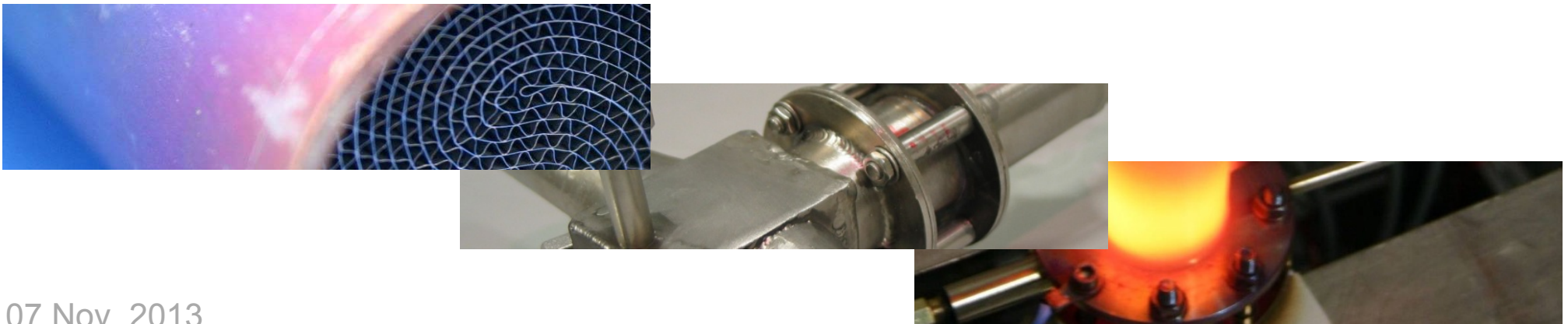


Design and Demonstration of an Ethanol Fuel Processor for HT-PEM Fuel Cell Applications

AIChE Annual Meeting 2013
Fuel Processing for Hydrogen Production



07 Nov. 2013



Overview

- Introduction
- Process Simulation
- Heat Integration Analysis
- Catalyst Selection
- Component Development
- Fuel Processor Demonstration
- Outlook

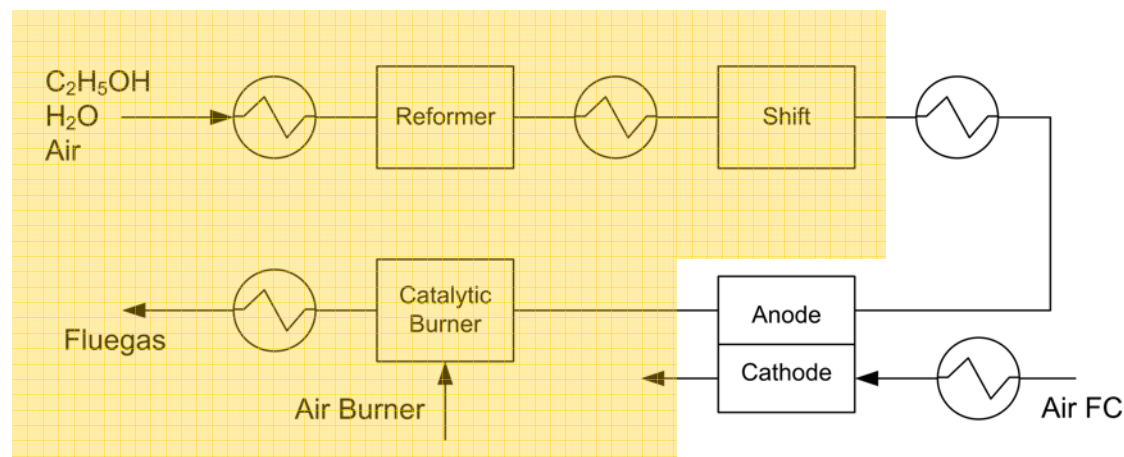
Application

- Hydrogen generation for small scale fuel cell systems ($P_{el} = 200 - 500 \text{ W}$)
- HT PEM fuel cell
- Off grid stationary power supply
- Backup power
- Leisure and security markets

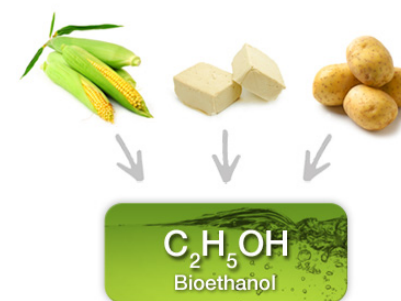
Fuel Bioethanol (C_2H_5OH)

- CO_2 neutral
- Good portability
- High energy density
- Good storage capability

Fuel processor boundary



Flow sheet of reformer fuel cell system



Source www.lacus.ch

Requirements Fuel Processor

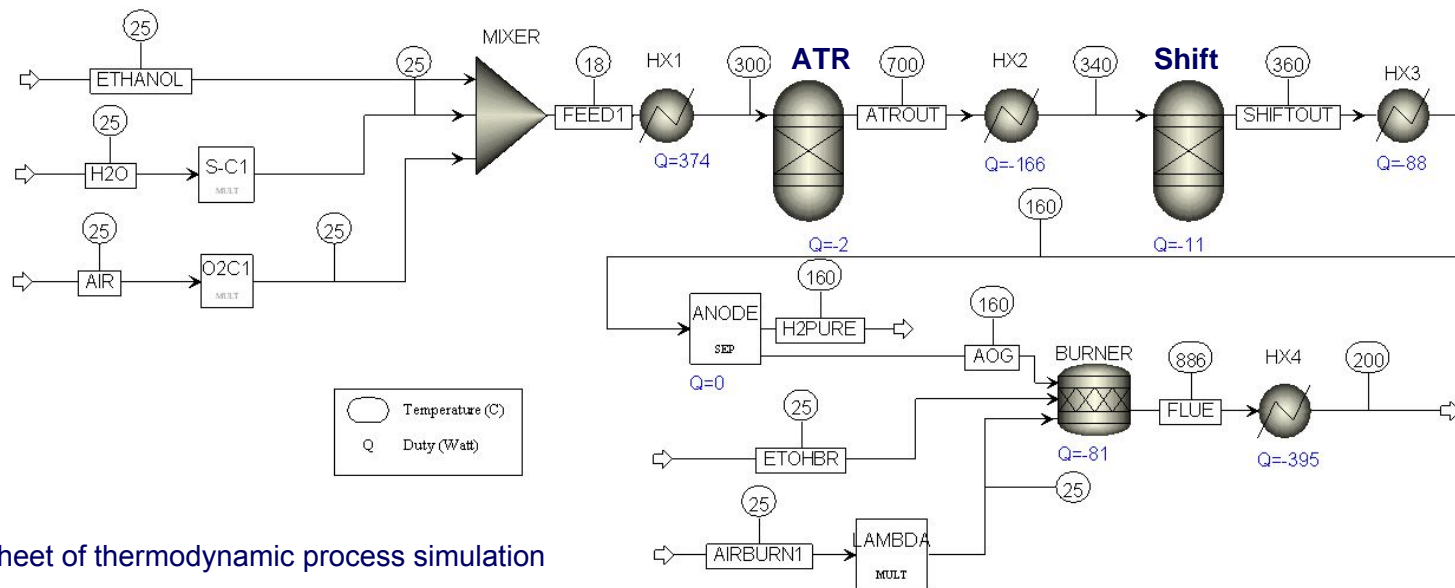
- $P_{H_2} = 600 - 1500 \text{ W}$
- HT PEM FC suitable reformat gas quality ($CO \leq 1 \%$)
- Fast start up
- High robustness
- Potential of low cost manufacturing
- Low pressure drop

→ Autothermal Reforming of Bioethanol

Approach

- Parameter variation
- Reformate gas composition
- Definition heat streams and heat demand
- Carbon and side product formation
- Definition of basic operation point

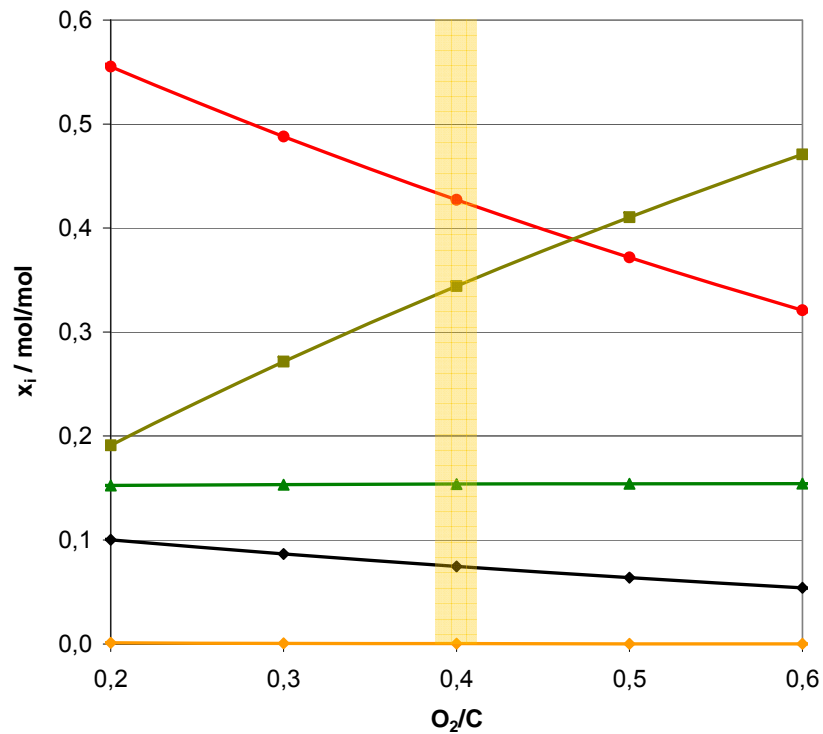
| Parameter | Interval | Step | Basic Operation Point |
|------------------------------|-----------|------|-----------------------|
| $T_{ATR} / ^\circ\text{C}$ | 500 - 800 | 25 | 700 |
| $O_2/C / -$ | 0 - 1.5 | 0.1 | 0.4 |
| $S/C / -$ | 0 - 5 | 0.25 | 2.75 |
| $T_{Shift} / ^\circ\text{C}$ | 200 - 400 | 25 | 300 |



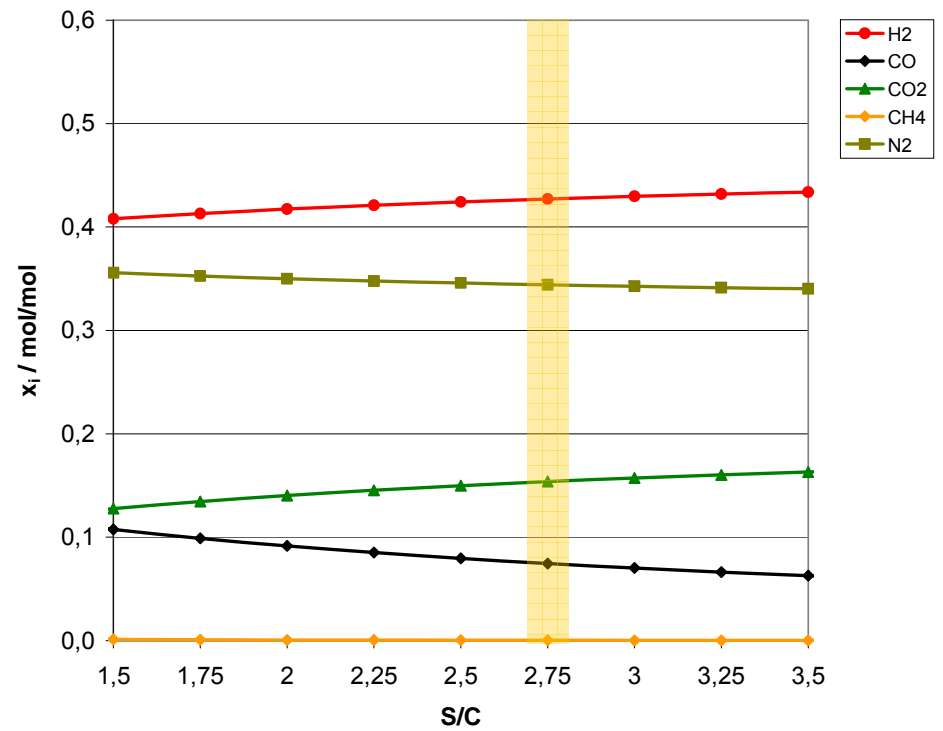
Flow sheet of thermodynamic process simulation

○ Temperature (C)
Q Duty (Watt)

Product gas composition (example ATR out)

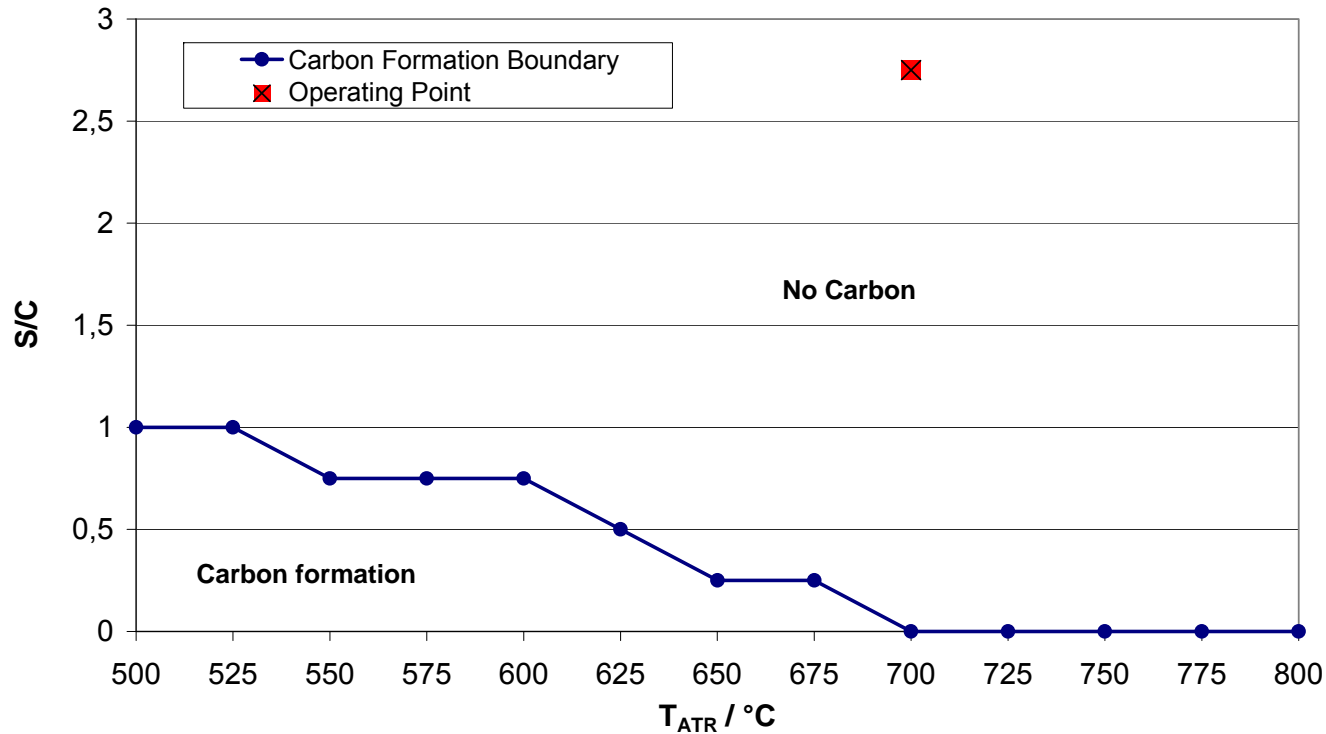


Equilibrium, $T_{ATR} = 700\text{ }^{\circ}\text{C}$, $S/C = 2.75$



Equilibrium, $T_{ATR} = 700\text{ }^{\circ}\text{C}$, $O_2/C = 0.40$

Thermodynamic Potential of Carbon Formation



Carbon formation boundaries of EtOH reforming (O₂/C = 0.4)

Aspen settings for solid carbon

| Parameter | Setting |
|---|---|
| Method | IDEAL |
| Stream Class | Mix CISLD |
| Reactor type | Gibbs-reactor (possible products gas phase & pure solid) |
| Consideration of carbon formation by homogeneous gas phase reaction | |

Approach

- Basic operation point
- Simulation results
(heat streams, temperatures)
- Pinch Point Analysis

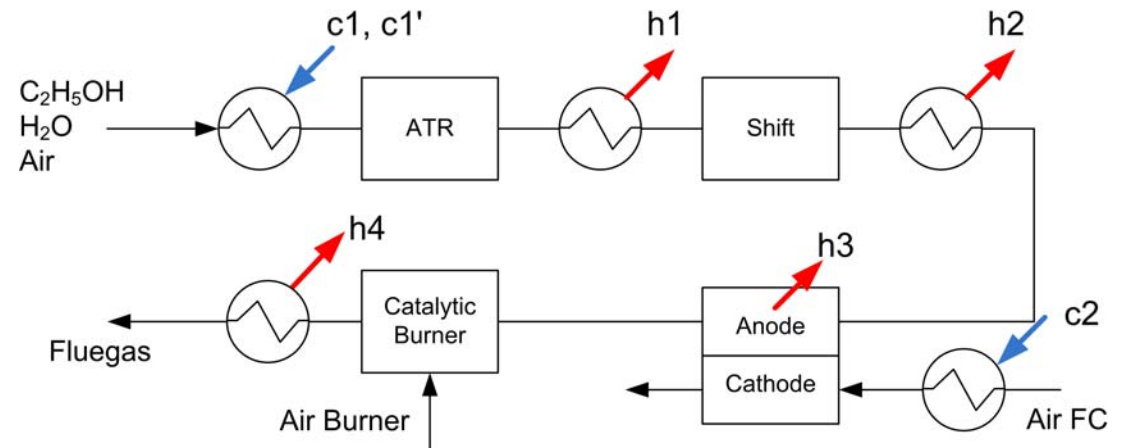
Main System Layout Targets

Minimization of

- Heat exchangers
- Heat exchangers with high thermal stress ($> 500\text{ }^{\circ}\text{C}$)
- Heat exchangers with internal evaporation (mixing of educts)

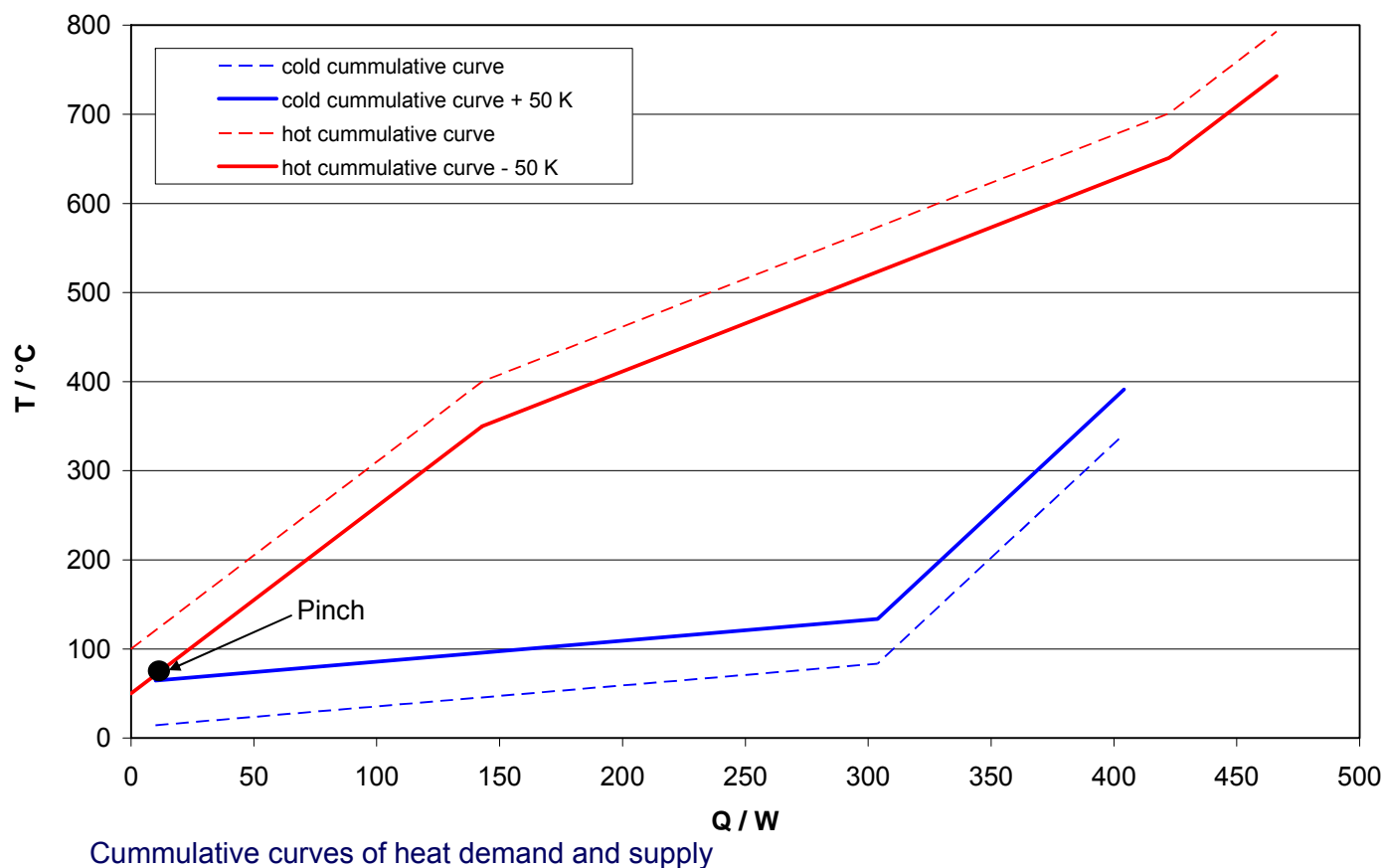
Maximization of

- Variance for setting of main temperatures
- Internal fulfilment of heat demand



Pinch Point Analysis

for streams c1', c1, h1 and h4

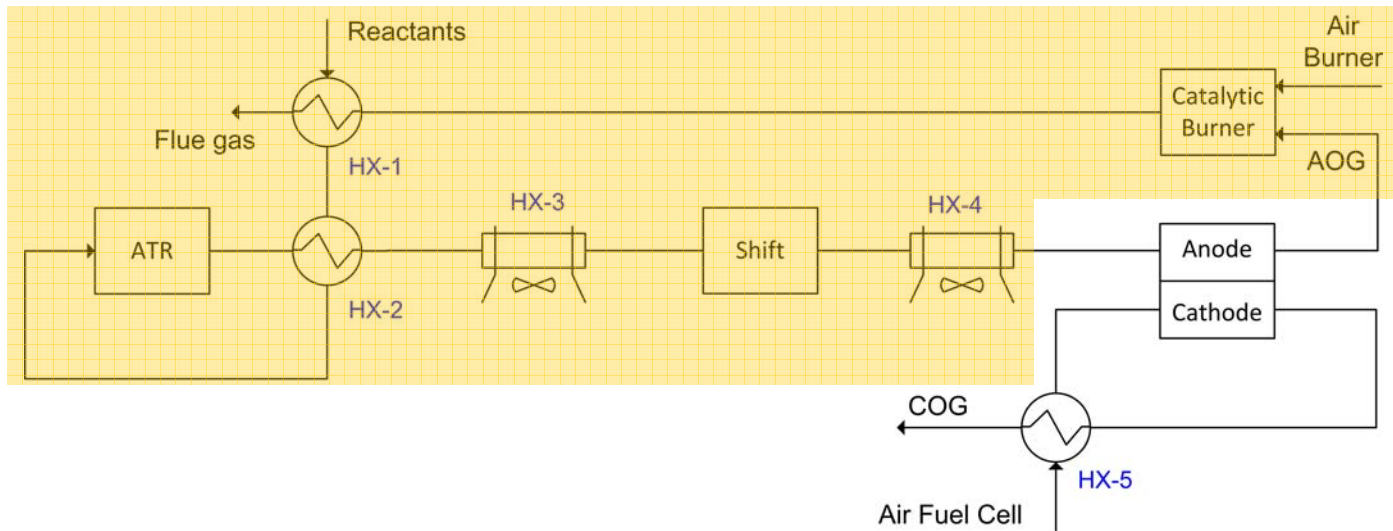


| Stream | $T_{in} / ^\circ C$ | $T_{out} / ^\circ C$ | Q / W |
|--------|---------------------|----------------------|---------|
| c1' | 14 | 84 | 294 |
| c1 | 84 | 341 | 100 |
| h1 | 793 | 100 | -330 |
| h4 | 700 | 400 | -136 |

Resulting System Flow Sheet

- Reactants (C_2H_5OH , H_2O , Air) completely premixed
- 4 heat exchangers (two coupled) for fuel processor
- $T_{Shift,in}$ and $T_{Anode,in}$ freely adjustable

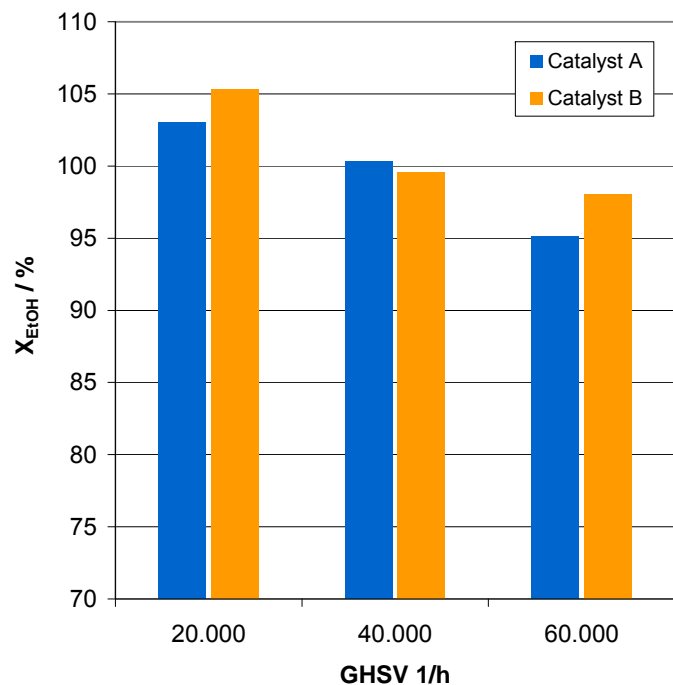
Fuel processor boundary



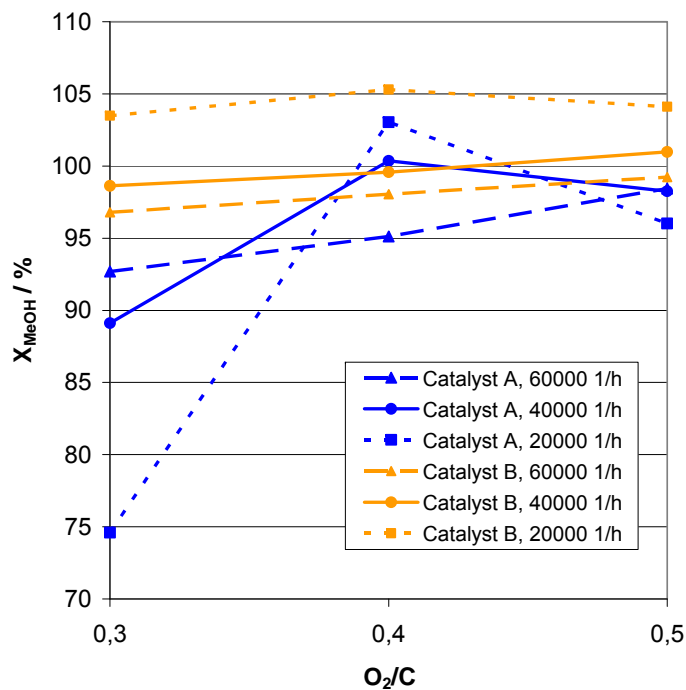
Flow Sheet Fuel Cell System

Screening

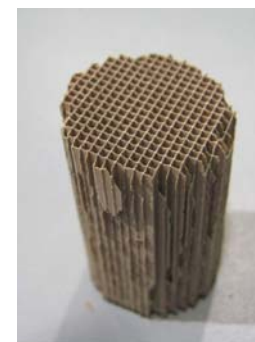
- Precious metal catalysts
- Ceramic monolith



EtOH conversion as function of GHSV
(S/C = 2.75, O₂/C = 0.40)



EtOH conversion as function of O₂/C and GHSV
(S/C = 2.75)



$$X_{EtOH} = \frac{(\dot{n}_{EtOH,out} - \dot{n}_{EtOH,in})}{\dot{n}_{EtOH,in}}$$

$\dot{n}_{EtOH,out}$ calculated by means
of C-atom balance



ATR

- Precious metal catalyst
- GHSV = 50,000 1/h
- Ceramic monolith (600 cpsi)
- Adiabatic reactor

Shift

- Precious metal catalyst
- GHSV = 15,000 1/h
- Ceramic monolith (600 cpsi)
- Adiabatic reactor

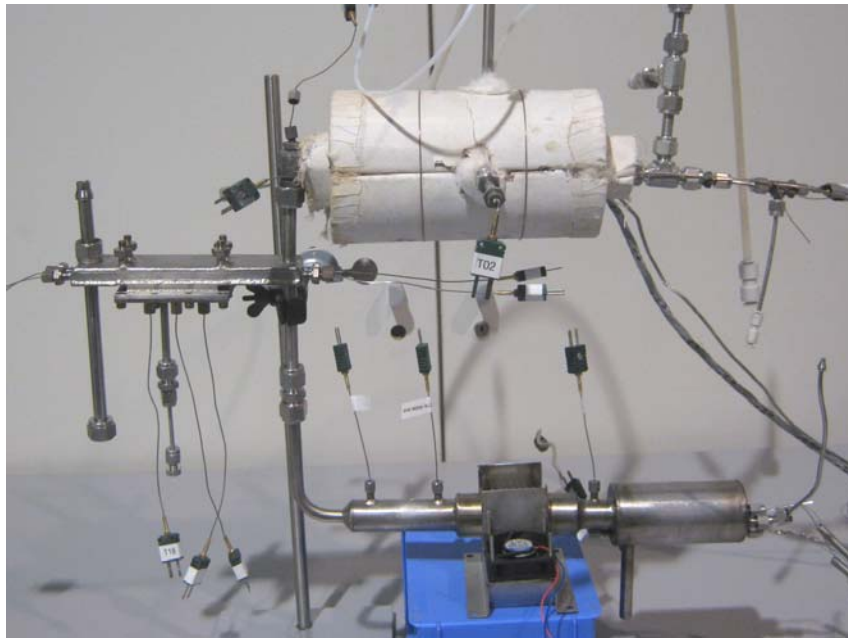
Burner

- Precious metal catalyst
- GHSV = 25,000 1/h
- Ceramic monolith (600 cpsi)
- Electrical heater / glow plug (alternative)
- Evaporation zone with metal fibre structure
- Suitable for ethanol and AOG

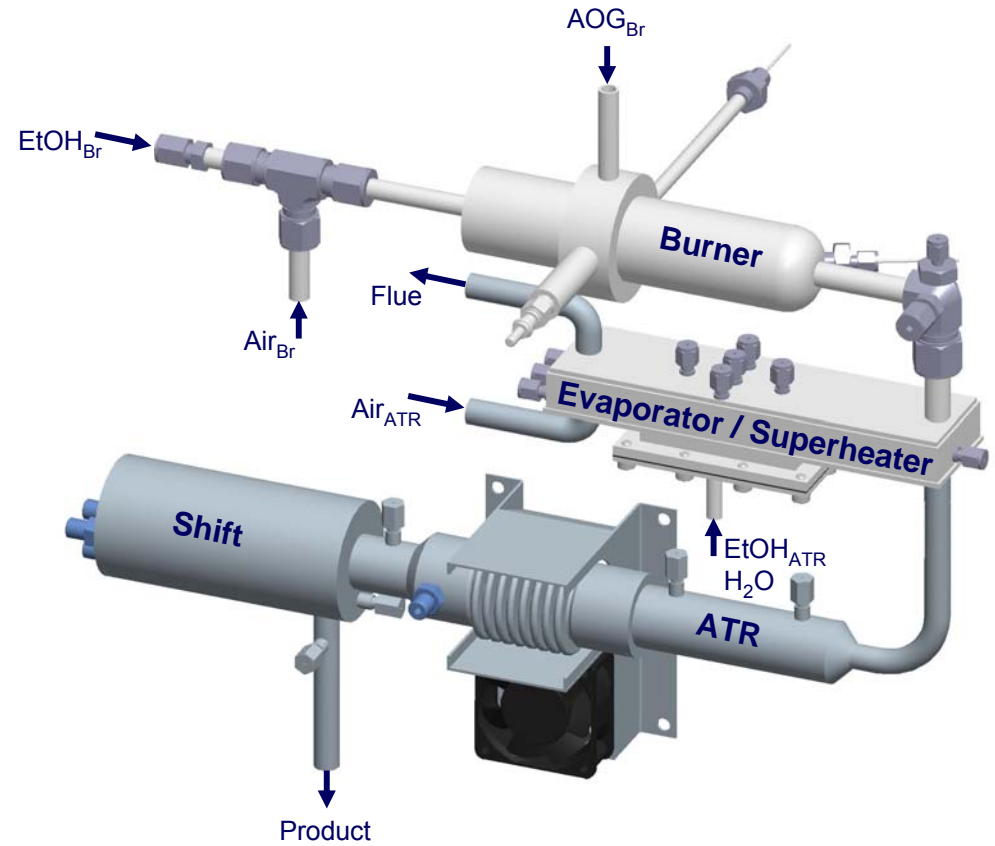
Evaporator Superheater Unit

- Internal cooling fins
- Counter current flow
- Flue gas as heat source
- Evaporation zone with metal foam structure
- Superheating zone

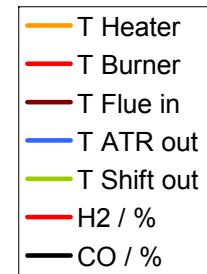
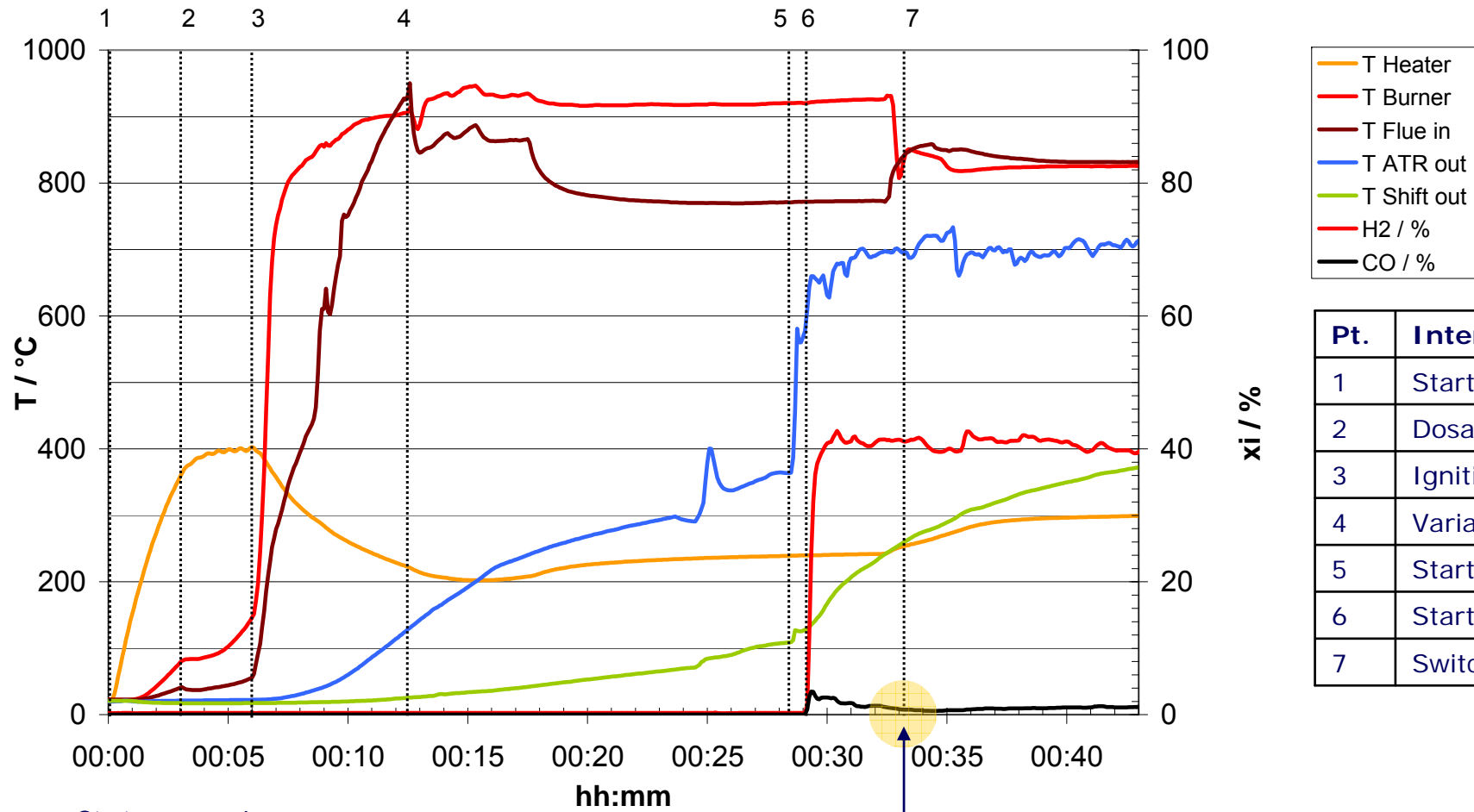
Laboratory Fuel Processor



Fuel processor assembly equipped with thermocouples



Start up process

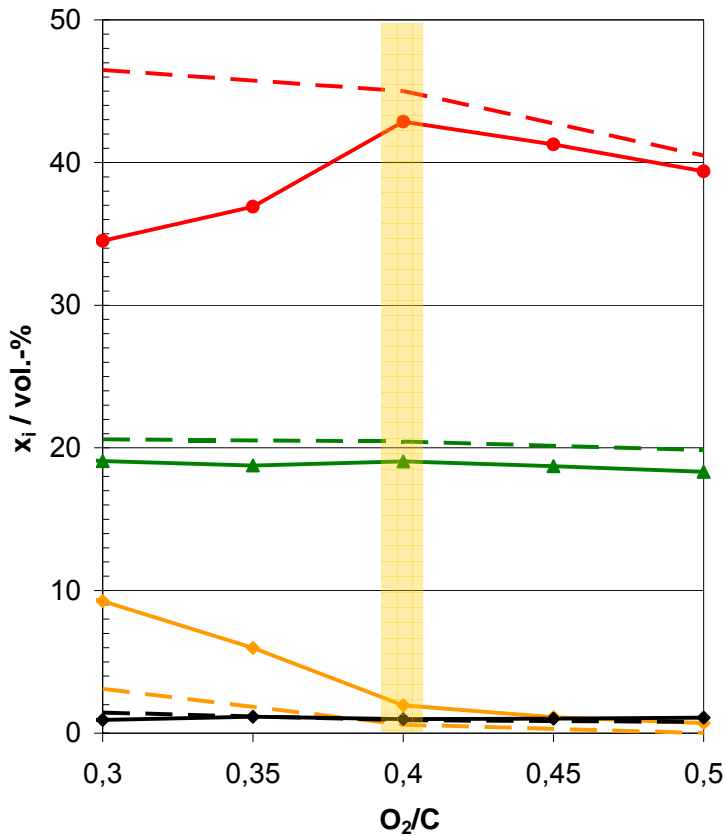


| Pt. | Interval |
|-----|-------------------------------|
| 1 | Start Heater |
| 2 | Dosage EtOH burner |
| 3 | Ignition burner |
| 4 | Variation load burner |
| 5 | Start H ₂ O dosage |
| 6 | Start reforming |
| 7 | Switch to AOG |

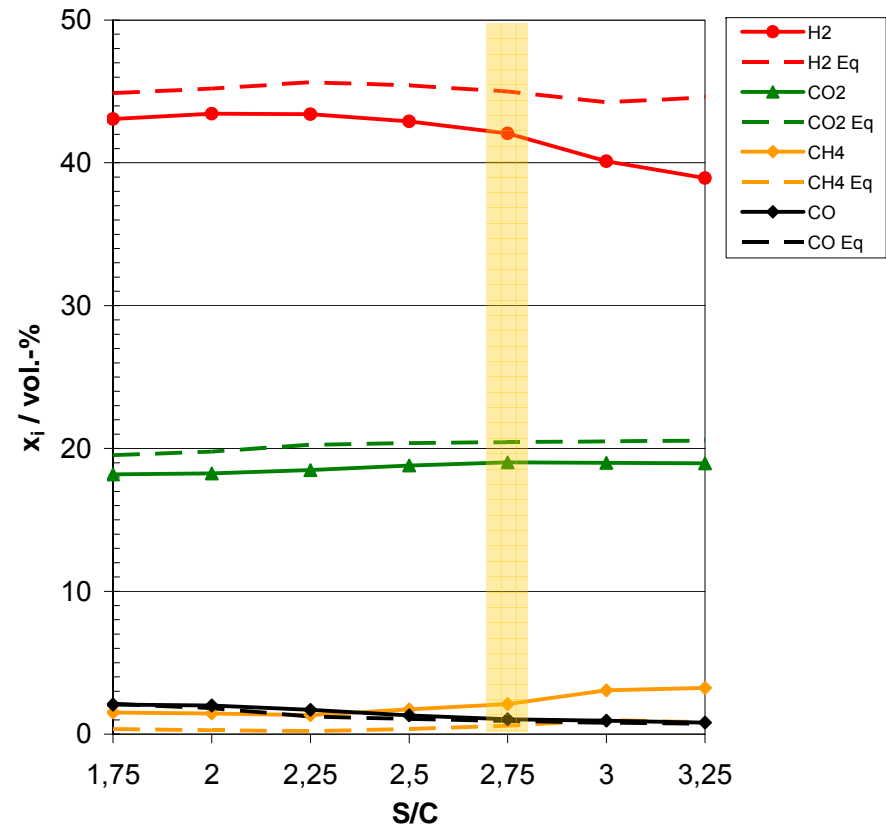
$x_{CO} < 2\%$

Gas composition shift out

- Variations of O_2/C and S/C



x_i as function of O_2/C (S/C = 2.75), measurement vs. equilibrium, dry

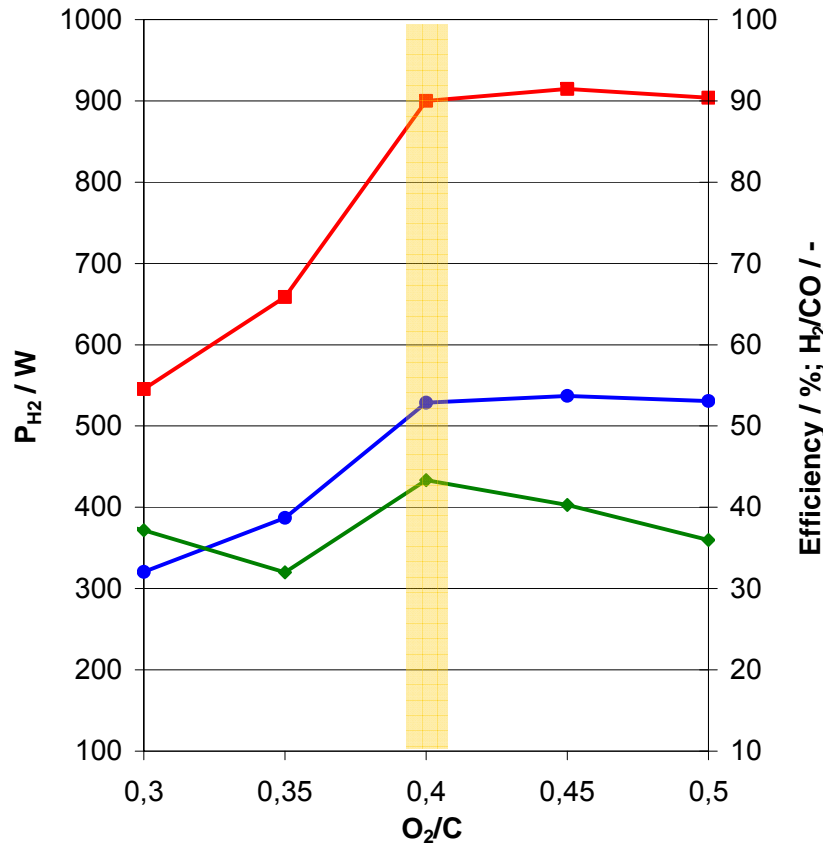


x_i as function of S/C ($O_2/C = 0.4$), measurement vs. equilibrium, dry

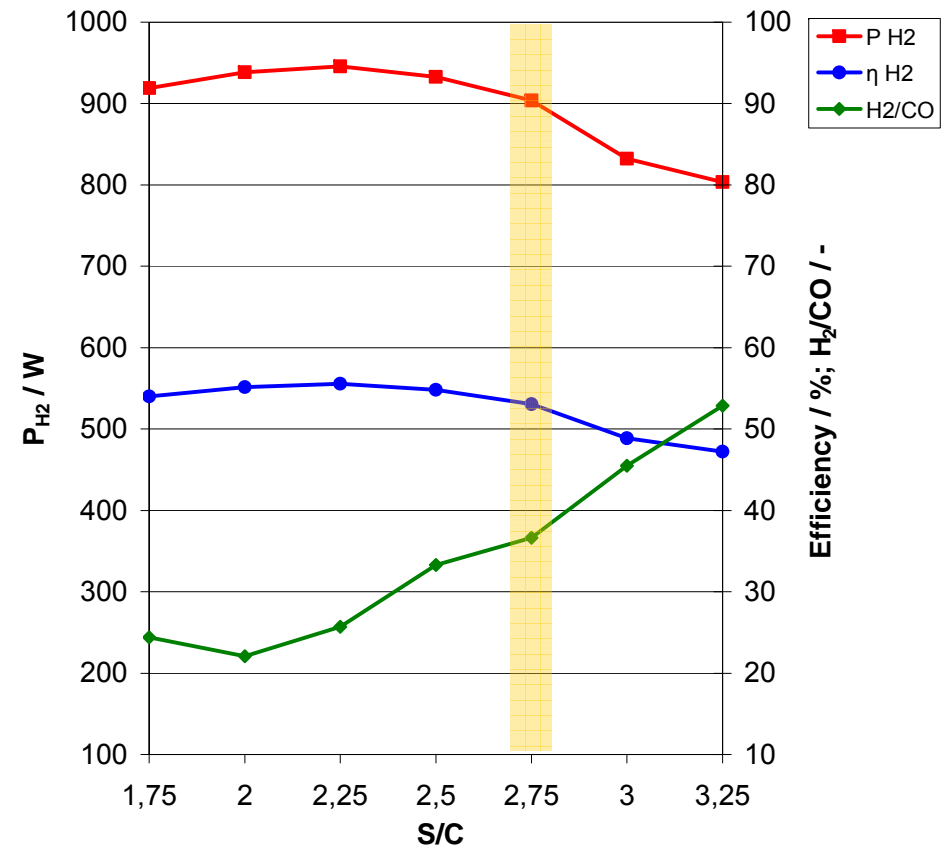
Power output / efficiency steady state

$$\eta_{H_2} = \frac{P_{H_2}}{P_{EtOH,ATR} + P_{Burn} + P_{AOG}}$$

P_{H_2} calculated by means of N_2 -atom balance



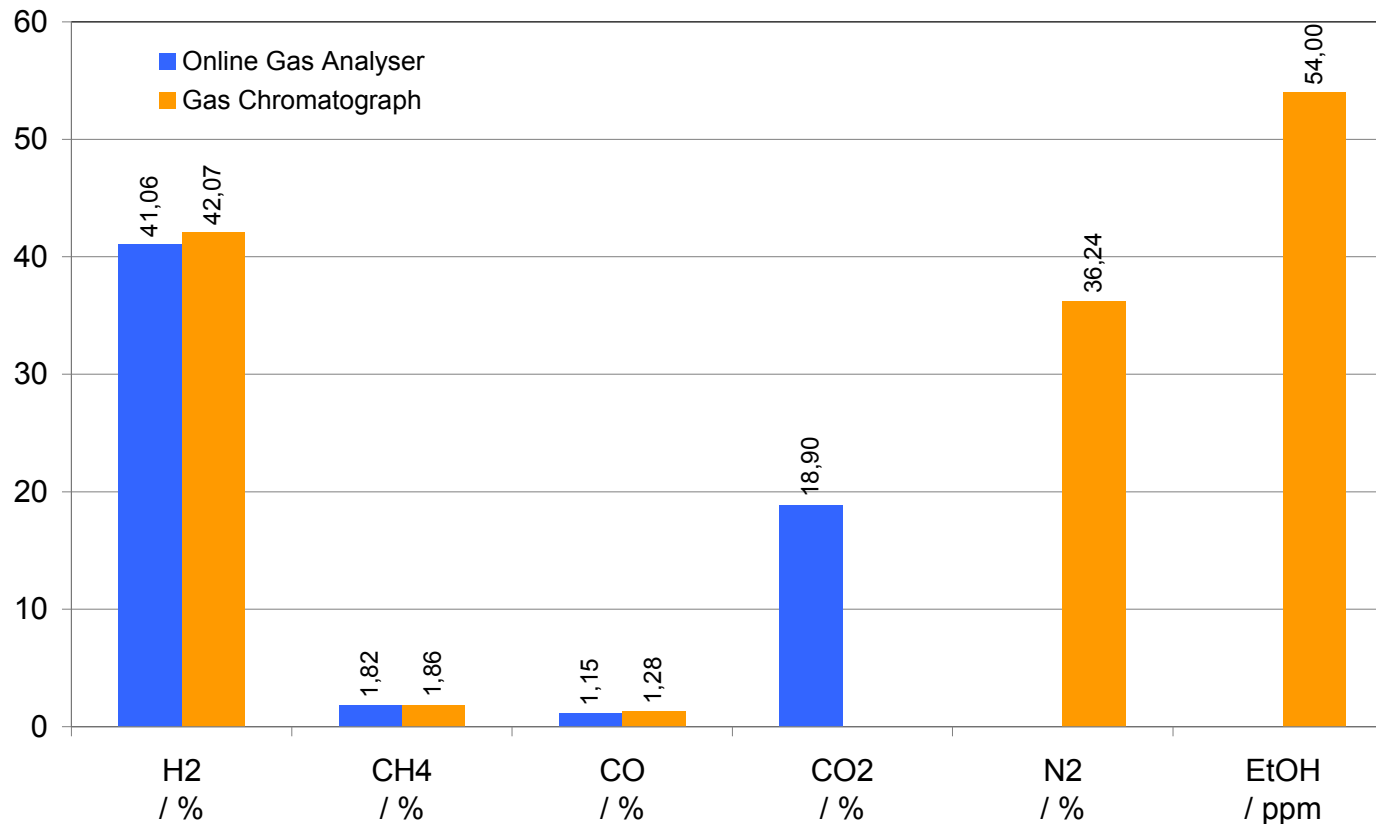
Performance data as function of O_2/C ($S/C = 2.75$)



Performance data as function of S/C ($O_2/C = 0.4$)

Gas composition shift out

- Comparison Online Gas Analyser (Rousemount Analytical NGA 2000, MLT 4) vs. Gas Chromatograph (Agilent Micro GC 3000A)



x_i of basic operation point (O_2/C , $S/C = 2.75$), online GA vs. GC, dry basis

Calibrated Components for GC

| Comp. | Lower limit / % | Upper limit / % |
|---------------------------------|-----------------|-----------------|
| He | 0,356 | 1,663 |
| H2 | 35,87 | 81,363 |
| O2 | 0,051 | 20,5 |
| N2 | 0,524 | 89,93 |
| CH4 | 0,3195 | 88,2 |
| CO | 0,1972 | 49,3 |
| Ethan | 0,0104 | 14,0 |
| Propan | 0,0102 | 3,01 |
| iso-Butan | 0,0104 | 0,539 |
| n-Butan | 0,0099 | 0,803 |
| N-pentan | 0,0107 | - |
| NH3 | 0,0487 | 1,044 |
| N-Hexan | 0,0107 | - |
| C ₂ H ₄ O | 0,0983 | 1,015 |
| MeOH | 0,165 | - |
| EtOH | 0,0103 | 0,098 |

Development Status

| Parameter | Basic Operation Point |
|-------------------------------------|-----------------------|
| $m_{\text{EtOH}} / \text{g/h}$ | 160 |
| $\text{O}_2/\text{C} / -$ | 0.42 |
| $\text{S}/\text{C} / -$ | 2.75 |
| $T_{\text{ATR}} / ^\circ\text{C}$ | 650 – 700 |
| $T_{\text{Shift}} / ^\circ\text{C}$ | 380 – 400 |
| $\text{H}_2 / \%$ | 42,0 |
| $\text{CO} / \%$ | 0,9 |
| $\text{CO}_2 / \%$ | 19,0 |
| $\text{CH}_4 / \%$ | 2,0 |
| EtOH / ppm | 54 (GC meas.) |
| $\text{N}_2 / \%$ | 36,1 (calculated) |

| Performance Data | Status | Target |
|---|-----------|------------|
| Power output $P_{\text{H}_2} / \text{W}$ | 900 | 600 - 1500 |
| Efficiency $\eta_{\text{H}_2} / \%$ | 55 | 70 |
| $X_{\text{EtOH}} \text{ ATR} / \%$ (calculated) | ~ 100 | 100 |
| Gasquality, $\text{CO} / \%$ | 1.0 – 1.5 | < 1.0 |
| Start up time / Min | ~ 30 | < 15 |
| Pressure drop / mbar | 15 - 20 | 20 |

Issues to be addressed

- Long term test
- Reduction start up time
- Optimization evaporator
- Enhancing efficiency
- Optimization temperature control shift
- Coupling with HT-PEM fuel cell

Thanks!

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PROJEKTRÄGER FÜR DAS



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